

DESCRIPTION

SWITCHING POWER-SUPPLY UNIT

Technical Field

The present invention relates to methods for controlling a switching power supply including a plurality of switching elements and, more particularly, to control methods not requiring an oscillation circuit.

Background Art

Control procedures called PWM (Pulse Wide Modulation) systems and PFM (Pulse Frequency Modulation) systems are generally available as methods for controlling switching elements in switching power supplies (See Non-Patent Document 1).

PWM systems are systems for controlling the ratio of an ON-period of a switching element to a switching period, and generally, the switching period is constant. In a case where a plurality of switching elements is provided, the ON-period ratios of the switching elements are equal to each other or inverted with respect to each other.

PFM systems are systems for controlling a switching frequency, and generally, an ON-period ratio of a switching element is constant. In a case where a plurality of switching elements is provided, the relationships between the ON-period ratios and the switching frequencies of the switching elements are equal to each other.

Non-Patent Document 1: Electrical Engineering Handbook
(Sixth Edition) by The Institute of Electrical Engineers of
Japan, February 20, 2001, Vol. 20, Chapter 9, Section 2
Switching Regulator, pp851-852.

Disclosure of the Invention

Problems to be Solved by the Invention

In known technologies, when a plurality of switching elements is provided, an oscillation circuit is also provided. A plurality of driving signals is produced based on an oscillation signal of the oscillation circuit, and the driving signals are transmitted to control terminals of the switching elements. Thus, if a delay time or an advanced time is generated in a path for transmitting the driving signals or a driving circuit, a phenomenon in which the plurality of switching elements is in an ON-state at the same time occurs even though the plurality of switching elements connected in series with each other must be driven in order. This phenomenon may not only prevent normal operation but may also destroy a power-supply unit due to an overcurrent or the like, thus significantly reducing reliability.

Thus, in order to avoid the phenomenon of the plurality of switching elements being in the ON-state at the same time, a dead time in which the plurality of switching elements is in an OFF-state at the same time is provided. However,

since the dead time does not contribute to voltage conversion, providing a dead time whose length is unnecessarily long constitutes a factor to reduce the power conversion efficiency. In addition, since the ON-period ratio and the switching frequency change in PWM systems and PFM systems, respectively, it is very difficult to set the dead time properly, and a complicated configuration is required.

In addition, in known technologies, obviously, an oscillation circuit functioning as a standard is required.

Furthermore, in known technologies, control to stabilize an output voltage by changing an ON-period of a switching element functioning as a standard is performed. For example, keeping an output voltage constant is the only one condition for the control.

An object of the present invention is to solve problems due to a plurality of switching elements being in an ON-state at the same time, to be capable of setting a plurality of conditions for control to satisfy predetermined conditions, and to provide a switching power-supply unit not requiring an oscillation circuit functioning as a standard.

Means for Solving the Problems

(1) A switching power-supply unit according to the present invention including an inductor or a transformer and a plurality of switching elements switching a current

flowing in the inductor or the transformer and converting power by turning on and off the switching elements is characterized by including a switching control circuit that turns on the next switching element in accordance with a change of a voltage or a current generated by turning off of a switching element in an ON-state, that sequentially turns on and off the switching elements in association with each other, that repeats a series of on-off operations of the switching elements periodically, that determines an ON-period of each of the switching elements in accordance with a condition independently provided for each of the switching elements, and that controls the ON-period of each of the switching elements.

(2) The switching power-supply unit of (1) according to the present invention is characterized in that a dead time in which two consecutive switching elements from among the plurality of switching elements are turned off is provided between ON-periods of the two switching elements and in that the dead time is arranged in accordance with a delay time from turning off of the switching element in the ON-state and turning on of the next switching element.

(3) The switching power-supply unit of (2) according to the present invention is characterized in that the dead time is set such that the switching element is turned on when a voltage across the switching element becomes zero or

reduces to near zero.

(4) The switching power-supply unit of (1) to (3) according to the present invention is characterized by turning on the next switching element using a voltage at the inductor or the transformer generated due to turning off of the switching element in the ON-state from among the plurality of switching elements.

(5) The switching power-supply unit of (1) to (4) according to the present invention is characterized in that the switching control circuit detects an output voltage to a load to determine the ON-period in accordance with the output voltage.

(6) The switching power-supply unit of (1) to (4) according to the present invention is characterized in that the switching control circuit detects a change or a polarity of a voltage generated at the inductor or the transformer to determine the ON-period.

(7) The switching power-supply unit of (1) to (4) according to the present invention is characterized in that the switching control circuit detects the current flowing in the inductor or the transformer to determine the ON-period.

(8) The switching power-supply unit of (1) to (4) according to the present invention is characterized in that the switching control circuit detects a voltage across the switching element to determine the ON-period.

(9) The switching power-supply unit of (1) to (4) according to the present invention is characterized in that the switching control circuit detects a current flowing in the switching element to determine the ON-period.

(10) The switching power-supply unit of (9) according to the present invention is characterized in that the switching control circuit determines the ON-period of the switching element such that the switching element is turned off when the current flowing in the switching element becomes zero or reaches near zero.

Effects of the Invention

(1) According to the present invention, since turning off of a switching element in an ON-state causes the next switching element to be turned on, inconvenience of two switching elements being in an ON-state at the same time basically does not occur, thus improving the reliability of a switching power-supply unit.

In addition, in known technologies, control to stabilize an output by changing an ON-period of a switching element functioning as a standard is performed, and only one condition is provided for controlling the output voltage. In the present invention, however, two or more conditions, that is, at most conditions whose number corresponds to the number of switching elements, can be established.

In addition, the switching frequency is determined in

accordance with the accumulation of ON-pulses of a switching element, and an ON-period of each switching element is set. Thus, an oscillation circuit is not required.

(2) According to the present invention, a dead time based on a delay time of turning on and off of switching elements is arranged between ON-periods of two consecutive switching elements from among the plurality of switching elements, and the reliability of the switching power-supply unit due to the plurality of switching elements turning on at the same time is improved. In addition, since the dead time is set in accordance with the delay time before turning on, the dead time can be properly set easily and the dead time is not unnecessarily increased or decreased even if the switching frequency and the ON-period ratio changes due to a change in the ON-period of each switching element. Thus, the power conversion efficiency can be kept high.

(3) According to the present invention, since the switching element is turned on when the voltage across the switching element becomes zero or reduces to near zero, the switching loss can be significantly reduced and high efficiency can be achieved due to a zero-voltage switching operation of turning on at zero voltage.

(4) According to the present invention, since the switching control circuit turning on the next switching element using the voltage at the inductor or the transformer

generated due to turning off of a switching element in an ON-state from among the plurality of switching elements is provided, a voltage signal generated at the inductor or the transformer can be easily captured as a trigger signal and the switching element can be used as a driving voltage. Thus, a simple circuit structure can be achieved.

(5) According to the present invention, since an output voltage to a load is detected to determine the ON-period in accordance with the voltage, a constant-voltage power-supply unit can be easily configured.

(6) According to the present invention, since a change (falling and rising) or the polarity of the voltage generated at the transformer is detected to determine the ON-period of the switching element, a voltage signal generated at the transformer can be easily used as a trigger signal. Thus, a simple circuit structure can be achieved.

(7) According to the present invention, since the current flowing in the transformer is detected to determine the ON-period, for example, a conduction period of a rectifier diode and the ON-period of the switching element can be set equal to each other. Thus, an effective current and the peak value of a current flowing in the rectifier diode and the transformer can be reduced, and the conduction loss is thus reduced.

(8) According to the present invention, since the

voltage across the switching element is detected to determine the ON-period, the ON-state and the OFF-state of the switching element can be accurately determined, and this can be easily used as a trigger signal.

(9) According to the present invention, since the switching control circuit detects the current flowing in the switching element to determine the ON-period, the state of the switching element can be accurately determined and the switching element can be controlled. Thus, a necessary and appropriate dead time can be provided.

(10) According to the present invention, since the switching control circuit turns off the switching element when the current flowing in the switching element becomes zero or reaches near zero, the switching loss can be significantly reduced due to a zero-current switching operation of turning on at zero current. Thus, high efficiency can be achieved.

Brief Description of the Drawings

[Fig. 1] Fig. 1 includes a circuit diagram and a waveform chart of a switching power-supply unit according to a first embodiment.

[Fig. 2] Fig. 2 includes a circuit diagram and a waveform chart of a switching power-supply unit according to a second embodiment.

[Fig. 3] Fig. 3 includes a circuit diagram and a waveform

chart of a switching power-supply unit according to a third embodiment.

[Fig. 4] Fig. 4 includes a circuit diagram and a waveform chart of a switching power-supply unit according to a fourth embodiment.

[Fig. 5] Fig. 5 includes a circuit diagram and a waveform chart of a switching power-supply unit according to a fifth embodiment.

Reference Numerals

- T - transformer
- Lp - primary winding
- Ls - secondary winding
- Vi - input power supply
- Q1 - first switching element
- Q2 - second switching element
- Q3 - third switching element
- Ds1 to Ds3 - rectifier diode
- C1 - first smoothing capacitor
- C2 - second smoothing capacitor
- C3 - third smoothing capacitor
- CNT1 - first switching control circuit
- CNT2 - second switching control circuit
- CNT3 - third switching control circuit
- Vo1 - first output voltage
- Vo2 - second output voltage

Vo3 - third output voltage
OUT1 - first output terminal
OUT2 - second output terminal
OUT3 - third output terminal
Lr - inductor
Cr - capacitor

Best Mode for Carrying Out the Invention

A switching power-supply unit according to a first embodiment will be described with reference to Fig. 1. Part (A) of Fig. 1 is a circuit diagram of the switching power-supply unit, and part (B) is an illustration showing the relationship between the waveform of each section of the switching power-supply unit and time.

In part (A) of Fig. 1, Vi denotes an input power supply, and T denotes a transformer. A first switching element Q1 is connected to a primary winding Lp of the transformer T. For a secondary winding Ls of the transformer T, a first rectification and smoothing circuit constituted by a rectifier diode Ds1 and a smoothing capacitor C1 is provided. Also, a second rectification and smoothing circuit constituted by a rectifier diode Ds2, a second switching element Q2, and a second smoothing capacitor C2 is provided. In addition, a third rectification and smoothing circuit constituted by a rectifier diode Ds3, a third switching element Q3, and a third smoothing capacitor C3 is provided.

A first switching control circuit CNT1 on/off-controls the first switching element Q1, a second switching control circuit CNT2 on/off-controls the second switching element Q2, and a third switching control circuit CNT3 on/off-controls the third switching element Q3. In the figure, a broken line entering each of the switching control circuits CNT1, CNT2, and CNT3 schematically indicates a trigger path, and a solid line entering each of the switching control circuits CNT1, CNT2, and CNT3 schematically indicates a feedback path.

The first switching control circuit CNT1, from among the switching control circuits, receives a voltage (transformer voltage V_t) of the transformer T as a trigger, and turns on Q1 at a time when the drain voltage of Q1 falls. The first switching control circuit CNT1 also detects an output voltage V_{o1} of a first output terminal OUT1, and determines an ON-period of the first switching element Q1 such that V_{o1} is set to a predetermined voltage. In other words, the first switching control circuit CNT1 turns off Q1 at a time when the required ON-period of Q1 has passed.

The second switching control circuit CNT2 receives the voltage (transformer voltage) V_t of the transformer T as a trigger, and turns on the second switching element Q2 at a time when the voltage (transformer voltage V_t) of the transformer T inverts. Then, the second switching control circuit CNT2 detects a voltage V_{o2} of a second output

terminal OUT2, and determines an ON-period of the second switching element Q2 such that Vo2 is set to a predetermined voltage. In other words, the second switching control circuit CNT2 turns off Q2 at a time when the required ON-period of Q2 has passed.

The third switching control circuit CNT3 receives a drain voltage of the second switching element Q2 as a trigger, and turns on Q3 at a time when the drain voltage of Q2 rises. Then, the third switching control circuit CNT3 detects a voltage Vo3 of a third output terminal OUT 3, and determines an ON-period of the third switching element Q3 such that Vo3 is set to a predetermined voltage. In other words, the third switching control circuit CNT3 turns off Q3 at a time when the required ON-period of Q3 has passed.

In part (B) of Fig. 1, V_t represents the voltage (transformer voltage) of the transformer T, and Q1, Q2, Q3, and Ds represent the states of the first to third switching elements Q1 to Q3 and the first rectifier diode Ds1, respectively. Here, a high level represents an ON-state, and a low level represents an OFF-state.

(1) State 1 [t0-t1]

First, when the voltage (transformer voltage V_t) of the transformer T inverts at time t0, after the passage of a delay time τ_{td1} from the time t0, the gate voltage of the first switching element Q1 is turned to the high-level by

the first switching control circuit CNT1, and Q1 is thus turned on. The delay time τ_{td1} is set in accordance with a resonance period determined based on the primary inductance of the transformer T, the parasitic capacitance between the drain and source of Q1, and the like, such that Q1 is turned on at a time when the voltage between the drain and source of Q1 becomes zero. Thus, a zero-voltage switching operation of Q1 is performed, and the switching loss is significantly reduced.

Then, the first switching control circuit CNT1 determines an ON-period t_{on1} of Q1 such that the voltage of the voltage V_{o1} of the first output terminal OUT1 is set to a predetermined value. In other words, at time t_1 , that is, after the passage of $\tau_{td1} + t_{on1}$ from time t_0 , the first switching control circuit CNT1 turns the gate voltage of Q1 to the low-level. Thus, Q1 is turned off. The exciting energy of the transformer T is determined in accordance with the ON-period t_{on1} of Q1. As a result, the voltage of V_{o1} is determined.

(2) State 2 [t_1 - t_2]

When Q1 is turned off, the transformer voltage V_t inverts. The second switching control circuit CNT2 receives the voltage of the secondary winding L_s of the transformer T as a trigger signal, and turns the gate voltage of the second switching element Q2 to the high-level at time t_1

when the transformer voltage V_t inverts. Thus, Q2 is turned on after the passage of a delay time τ_{td2} from time t_1 . The delay time τ_{td2} is set in accordance with a resonance period determined based on the secondary inductance of the transformer T, the parasitic capacitance between the drain and source of Q2, and the like, such that Q2 is turned on at a time when the voltage between the drain and source of Q2 becomes zero. Thus, a zero-voltage switching operation of Q2 is performed.

The second switching control circuit CNT 2 determines an ON-period t_{on2} of Q2 such that the voltage of the voltage V_{o2} of the second output terminal OUT2 is set to a predetermined value. In other words, at time t_2 , that is, after the passage of $\tau_{td2} + t_{on2}$ from time t_1 , the second switching control circuit CNT2 turns the gate voltage of Q2 to the low-level.

(3) State 3 [t_2 - t_3]

Since the third switching control circuit CNT3 receives the drain voltage of Q2 as a trigger signal, when Q2 is turned off at t_2 , the third switching element Q3 is turned on after the passage of a delay time τ_{td3} from t_2 . The delay time τ_{td3} is set in accordance with a resonance period determined based on the secondary inductance of the transformer T, the parasitic capacitance between the drain and source of Q3, and the like, such that Q3 is turned on at

a time when the voltage between the drain and source of Q3 becomes zero. Thus, a zero-voltage switching operation of Q3 is performed.

The third switching control circuit CNT3 determines an ON-period t_{on3} of Q3 such that the voltage of the voltage V_{o3} of the third output terminal OUT3 is set to a predetermined value. In other words, at time t_3 , that is, after the passage of $t_{d3} + t_{on3}$ from time t_2 , the third switching control circuit CNT 3 turns the gate voltage of Q2 to the low-level.

(4) State 4 [t_3-t_0]

When Q3 is turned off, after the passage of a delay time t_{d4} from the time when Q3 is turned off, the first rectifier diode Ds1 is turned on. This is because Ds1 is turned on due to application of a forward voltage to Ds1 when both Q2 and Q3 are in the OFF-state with the relationship $V_{o1} > V_{o3} > V_{o2}$.

Then, the first switching control circuit CNT1 determines an ON-period t_{ond} of the rectifier diode Ds1 such that the voltage of the voltage V_{o1} of the first output terminal OUT1 is set to a predetermined value. When the current of Ds1 becomes zero and an inverse current is applied, the voltage of the transformer inverts at time t_0 . In other words, Ds1 is turned off at a time after the passage of $t_{d4} + t_{ond}$ from time t_3 , and the first switching

control circuit CNT1 turns the gate voltage of the first switching element Q1 to the high-level after the passage of the delay time t_{d1} from time t_0 . Time T_0 here is equal to the initial time t_0 .

As described above, by repeating a cycle T represented in part (B) of Fig. 1 as one cycle, predetermined voltages V_{o1} , V_{o2} , and V_{o3} can be obtained at the first to third output terminals OUT1 to OUT3, respectively.

With this structure, the next switching element is turned off in association with one switching element in an ON-state being turned off. Thus, in other words, an on/off state of each switching element changes in the order of the lapse of time based on causality. Since a delay time is inevitably required between turning off of one switching element in an ON-state and turning on of the next switching element, this delay time constitutes a dead time. Thus, the inconvenience of two switching elements being in the ON-state at the same time basically does not occur, thus improving the reliability of a switching power-supply unit. Furthermore, properly setting the dead time enables a zero-voltage switching operation and the like, and power conversion efficiency can be kept high without providing an unnecessarily long dead time.

In addition, since the accumulation of ON-pulses of a switching element functions as a switching frequency, an

oscillation circuit is not required. Furthermore, voltages of a plurality of outputs (three outputs in the first embodiment) whose number is equal to the number of switching elements can be stabilized independently. Although setting voltages of a plurality of output terminals to respective predetermined values is provided as conditions in this example, a current or the like, instead of a voltage, may be controlled as long as it can be controlled by an ON-period of a switching element. In other words, independent conditions whose number corresponds to the number of switching elements can be met.

Although turning off of the first and second switching elements Q2 and Q3 is detected based on the drain voltages of Q2 and Q3 in the example described above, turning off of the switching elements may be detected by detecting currents flowing in the switching elements. In addition, although the transformer voltage is detected based on the voltage of the secondary winding Ls of the transformer T as a trigger of Q2 in the example described above, a change in the transformer voltage may be detected based on the voltage of the primary winding Lp. Furthermore, instead of detecting falling of the transformer voltage, a change in the polarity of the transformer voltage may be detected.

In addition, although an operation of setting an output voltage to a predetermined value in the steady state is

described in the example described above, for example, by setting the maximum ON-period of each switching element at a transition time until an output voltage reaches a predetermined value, such as a starting time, a series of switching operations are repeated periodically, and a steady state is reached.

A switching power-supply unit according to a second embodiment will be described with reference to Fig. 2. Part (A) of Fig. 2 is a circuit diagram of the switching power-supply unit, and part (B) is an illustration showing the relationship between the waveform of each section of the switching power-supply unit and time.

In part (A) of Fig. 2, an inductor L_r is connected to the primary winding L_p of the transformer T . The second switching element Q_2 and a capacitor C_r are provided so as to form a closed loop together with the inductor L_r and the primary winding L_p . A rectification and smoothing circuit constituted by a rectifier diode D_s and a smoothing capacitor C_o is connected to the secondary winding L_s of the transformer T .

The first switching control circuit CNT1 on/off-controls the first switching element Q_1 , and the second switching control circuit CNT2 on/off-controls the second switching element Q_2 . In the figure, a broken line entering each of the switching control circuits CNT1 and CNT2

schematically indicates a trigger path, and a solid line entering each of the switching control circuits CNT1 and CNT2 schematically indicates a feedback path.

The first switching control circuit CNT1 receives an inverting time when the voltage (transformer voltage) of the transformer T rises as a trigger. The first switching control circuit CNT1 also detects an output voltage V_o , and controls the ON-period of the first switching element Q1 such that V_o is set to a predetermined voltage.

The second switching control circuit CNT2 receives an inverting time when the transformer voltage of the transformer T falls as a trigger. The second switching control circuit CNT2 also detects a voltage v_c across the capacitor C_r , and controls the ON-period of Q2 such that v_c is set to a predetermined voltage or v_c does not exceed the predetermined voltage.

In part (B) of Fig. 2, V_t represents the waveform of the transformer voltage, and Q1 and Q2 represent the states of the first and second switching elements Q1 and Q2, respectively. Here, a high-level represents an ON-state, and a low-level represents an OFF-state.

(1) State 1 [t_0 - t_1]

The first switching control circuit CNT1 receives a trigger signal at time t_0 , and after the passage of a predetermined delay time τ_{t1} , the first switching control

circuit CNT1 turns the gate voltage of Q1 to the high-level. Thus, Q1 is turned on. Since the output voltage V_o changes in accordance with the ON-period t_{on1} of the first switching element Q1, t_{on1} is determined such that a predetermined output voltage V_o can be obtained. In other words, at a time after the passage of $\tau t_1 + t_{on1}$ from time t_0 , the gate voltage of the first switching element Q1 is turned to the low-level, and Q1 is thus turned off.

(2) State 2 [$t_1 - t_0$]

When Q1 is turned off, the transformer voltage V_t inverts. After the passage of a delay time τt_2 , the second switching control circuit CNT2 turns the gate voltage of Q2 to the high-level using the inverting time of the transformer voltage V_t as a trigger. Thus, the second switching element Q2 is turned on.

Since the voltage v_c across the capacitor C_r changes in accordance with the ON-period t_{on2} of Q2, t_{on2} is determined such that v_c is set to a predetermined voltage. In other words, at a time after the passage of $\tau t_2 + t_{on2}$ from time t_1 , the second switching control circuit CNT2 turns the gate voltage of Q2 to the low-level. Thus, Q2 is turned off.

Since the transformer voltage V_t re-inverts when Q2 is turned off, after the passage of the delay time τt_1 from time t_0 , the first switching control circuit CNT1 turns the gate voltage of the first switching element Q1 to the high-

level using the re-inversion of the transformer voltage V_t as a trigger. Time t_0 here is equal to the initial time t_0 .

As described above, by repeating a cycle T shown in part (B) of Fig. 2 as one cycle, operation as a voltage-clamped flyback converter can be achieved. In this example, it is controlled such that the output voltage V_o to a load is kept constant and that the voltage v_c across the capacitor C_r is set to a stabilized voltage. In addition, properly setting the delay times t_1 and t_2 enables zero-voltage switching operations of Q_1 and Q_2 , thus significantly reducing the switching loss.

Although operation as a constant-voltage power-supply unit is described in the example described above, since V_o and v_c are detected to determine the ON-periods t_{on1} and t_{on2} of the switching elements Q_1 and Q_2 , respectively, the voltages V_o and v_c can be controlled to satisfy predetermined conditions by controlling t_{on1} and t_{on2} , respectively.

The first and second switching control circuits CNT1 and CNT2 may detect a voltage at the inductor L_r generated in accordance with turning off of Q_1 and Q_2 .

A switching power-supply unit according to a third embodiment will be described with reference to Fig. 3. Part (A) of Fig. 3 is a circuit diagram of the switching power-supply unit, and part (B) is an illustration showing the

relationship between the waveform of each section of the switching power-supply unit and time.

Unlike the case shown in Fig. 2, a tertiary winding L_t of the transformer T is provided and a rectification and smoothing circuit constituted by the rectifier diode D_{s2} and the smoothing capacitor C_2 is connected to the tertiary winding L_t in this example. The second switching control circuit CNT_2 detects the output voltage V_{o2} of the second output terminal OUT_2 and performs feedback control. The other structures are similar as in the second embodiment. This switching power-supply unit operates as a voltage-clamped flyback converter.

Thus, the output voltages V_{o1} and V_{o2} can be kept at predetermined voltages by controlling the ON-periods ton_1 and ton_2 of the first and second switching elements Q_1 and Q_2 by the first and second switching control circuits CNT_1 and CNT_2 , irrespective of the voltage of an input power supply v_i and a load current.

A switching power-supply unit according to a fourth embodiment will be described with reference to Fig. 4. Part (A) of Fig. 4 is a circuit diagram of the switching power-supply unit, and part (B) is an illustration showing the relationship between the waveform of each section of the switching power-supply unit and time.

As shown in part (A) of Fig. 4, the first switching

element Q1 and a capacitor Cr1 are connected to each other to form a closed loop together with the inductor Lr and the primary winding Lp of the transformer T. The first and second switching elements Q1 and Q2 are connected in series with each other, and the second switching element Q2 and a capacitor Cr2 are connected to each other to form another closed loop together with Lr and Lp. The rectifier diodes Ds1 and Ds2 are connected to secondary windings Ls1 and Ls2 of the transformer T, respectively, and they form a rectification and smoothing circuit together with the smoothing capacitor Co.

The first switching control circuit CNT 1 receives a time when the voltage (transformer voltage) of the transformer T rises as a trigger. The first switching control circuit CNT1 also detects the output voltage Vo, and controls the ON-period of the first switching element Q1 such that Vo is set to a predetermined voltage.

The second switching control circuit CNT2 receives a time when the transformer voltage of the transformer T falls as a trigger. The second switching control circuit CNT2 also detects the transformer voltage Vt of the transformer T, and turns off Q2 when Vt becomes zero.

In part (B) of Fig. 4, Vt represents the waveform of the transformer voltage, and it represents the waveform of a current flowing in the primary winding Lp of the transformer

T. Also, Q1 and Q2 represent the states of the first and second switching elements Q1 and Q2, respectively. Here, a high-level represents an ON-state, and a low-level represents an OFF-state.

(1) State 1 [t0-t1]

As shown in part (B) of Fig. 4, after the passage of the delay time τt_1 from time t0 when the transformer voltage V_t rises, the first switching control circuit CNT1 turns the gate voltage of Q1 to the high-level, and Q1 is thus turned on.

After turning on Q1, the ON-period ton_1 of Q1 is determined such that the output voltage V_o is set to a predetermined voltage. In other words, at a time after the passage of $\tau t_1 + ton_1$ from time t0, the gate voltage of Q1 is turned to the low-level. Thus, Q1 is turned off.

(2) State 2 [t1-t0]

When Q1 is turned off, the transformer voltage V_t falls. After the passage of the delay time τt_2 , the second switching control circuit CNT2 turns the gate voltage of Q2 to the high-level using the time when the transformer voltage V_t falls as a trigger. Thus, the second switching element Q2 is turned on.

When the transformer voltage V_t becomes zero, the second switching control circuit CNT2 turns the gate voltage of Q2 to the low-level. Thus, Q2 is turned off.

When Q2 is turned off, since the transformer voltage V_t re-rises, after the passage of the delay time t_{d1} , the first switching control circuit CNT1 turns the gate voltage of the first switching element Q1 to the high-level using the re-rising of the transformer voltage V_t as a trigger. Time t_0 here is equal to the initial time t_0 .

As described above, by repeating a cycle T shown in part (B) of Fig. 4 as one cycle, operation as a current-resonance half-bridge converter can be achieved.

According to this embodiment, when the transformer voltage V_t becomes zero, since the second switching element Q2 is turned off, the transformer current (the current it flowing in the primary winding L_p of the transformer T) whose phase is delayed with respect to the transformer voltage V_t allows the parasitic capacitances of Q1 and Q2 to be charged and discharged, thus enabling a zero-voltage switching operation of Q1. As a result, the switching loss of Q1 and Q2 can be significantly reduced. Although both the capacitors Cr1 and Cr2 are used in Fig. 4, similar advantages can be achieved by eliminating one of the capacitors Cr1 and Cr2.

A switching power-supply unit according to a fifth embodiment will be described with reference to Fig. 5. Part (A) of Fig. 5 is a circuit diagram of the switching power-supply unit, and part (B) is an illustration showing the

relationship between the waveform of each section of the switching power-supply unit and time.

Unlike the case shown in Fig. 2, the second switching control circuit CNT2 detects a current is flowing in the secondary winding L_s of the transformer T to determine the ON-period $ton2$ of the second switching element Q2.

In part (B) of Fig. 5, V_t represents the waveform of the transformer voltage, i_s represents the waveform of the current flowing in the secondary winding L_s of the transformer T. Q1 and Q2 represent the states of the first and second switching elements Q1 and Q2, respectively. Here, a high-level represents an ON-state, and a low-level represents an OFF-state.

(1) State 1 [t_0-t_1]

After the current i_s becomes zero and the delay time τ_{t1} passes, the first switching control circuit CNT1 turns the gate voltage of the first switching element Q1 to the high-level, and Q1 is thus turned on. The first switching control circuit CNT1 determines the ON-period $ton1$ of Q1 such that the output voltage V_o is set to a predetermined voltage, and turns off Q1 at time t_1 .

(2) State 2 [t_1-t_0]

Thus, the transformer voltage V_t inverts, and the second switching control circuit CNT2 uses the inversion as a trigger. After the passage of τ_{t2} , the second switching

control circuit CNT2 turns the gate voltage of the second switching element Q2 to the high-level. Thus, Q2 is turned on. When the current of the secondary winding Ls becomes zero, the second switching control circuit CNT2 turns the gate voltage of Q2 to the low-level using the current becoming zero as a trigger, and turns off Q2. Thus, the ON-period t_{on2} of Q2 is determined. This time is equal to the initial time t_0 described above.

By repeating the operation described above, operation as a constant-voltage power-supply unit can be achieved.

According to this embodiment, since the second switching element Q2 is turned off when the secondary winding current becomes zero, the conduction period of the rectifier diode Ds and the ON-period of Q2 are equal to each other. As a result, Q2 can be turned off when the current flowing in Q2 becomes zero, and a zero-current switching operation can be performed, thus significantly reducing the switching loss. In addition, an effective current and the peak value of the current flowing in the switching element Q2, the rectifier diode Ds, and the transformer T are reduced, thus reducing the conduction loss.